8053 measured reflections

 $R_{\rm int} = 0.033$

1650 independent reflections

1404 reflections with $I > 2\sigma(I)$

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5*a*-Androst-2-en-17-one

Datong Zhang^a* and Jun Liu^b

^aSchool of Chemical Engineering, Shandong Institute of Light Industry, Jinan 250353,
People's Republic of China, and ^bJinan Sijian (Group) Co. Ltd, Jinan 250031,
People's Republic of China

Correspondence e-mail: datong_zhang2006@yahoo.com.cn

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Key indicators: single-crystal X-ray study; T = 298 K; mean σ (C–C) = 0.005 Å; R factor = 0.048; wR factor = 0.122; data-to-parameter ratio = 9.1.

The title compound, $C_{19}H_{28}O$, is a useful intermediate for the synthesis of steroidal compounds. The molecular structure has normal bond lengths and angles. The crystal packing is stabilized by van der Waals forces.

Related literature

For related literature, see: Allen *et al.* (1987); Ambrogio & Paride (2000); D'Onofrio & Scettri (1985); Duax *et al.* (1976); Hanson *et al.* (1999).



Experimental

Crystal data

 $C_{19}H_{28}O$ $V = 1584.4 (7) Å^3$ $M_r = 272.41$ Z = 4Orthorhombic, $P2_12_12_1$ Mo K α radiationa = 6.4725 (17) Å $\mu = 0.07 \text{ mm}^{-1}$ b = 9.003 (2) ÅT = 298 (2) Kc = 27.190 (7) Å $0.41 \times 0.38 \times 0.10 \text{ mm}$

Data collection

Bruker SMART CCD area-detector diffractometer Absorption correction: multi-scan (SADABS; Sheldrick, 2004) $T_{min} = 0.973, T_{max} = 0.993$

Refinement

$$\begin{split} R[F^2 > 2\sigma(F^2)] &= 0.048 & 181 \text{ parameters} \\ wR(F^2) &= 0.122 & H\text{-atom parameters constrained} \\ S &= 1.09 & \Delta\rho_{max} &= 0.11 \text{ e } \text{\AA}^{-3} \\ 1650 \text{ reflections} & \Delta\rho_{min} &= -0.13 \text{ e } \text{\AA}^{-3} \end{split}$$

Data collection: *SMART* (Bruker, 2002); cell refinement: *SAINT* (Bruker, 2002); data reduction: *SAINT*; program(s) used to solve structure: *SHELXTL* (Sheldrick, 2001); program(s) used to refine structure: *SHELXTL*; molecular graphics: *SHELXTL*; software used to prepare material for publication: *SHELXTL*.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: HG2261).

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supplementary materials

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50-Androst-2-en-17-one

D. Zhang and J. Liu

Comment

Steroids occur widely in body tissues and have a large variety of physiological activities. Androsterone, a steroidal hormone, plays an important role in the development of male secondary sex characteristics during puberty and for promoting tissue and muscle growth. After elimination of the hydroxyl group at the 3-position of androsterone, 5α -androst-2-en-17-one was obtained as a useful intermediate for the synthesis of steroidal compounds. (D'Onofrio & Scettri., 1985; Hanson *et al.*, 1999). In this paper, we report the crystal structure of the title compound, (I).

In (I) (Fig. 1), all bond lengths and angles are normal (Allen *et al.*, 1987) and in a good agreement with those reported previously (Duax *et al.*, 1976). The values of torsion angles indicate that the A rings have halfchair conformations, the B and C rings have chair conformations, and the D rings have envelope conformations. The crystal packing is stabilized by van der Waals forces.

Experimental

Androsterone (17 mmol) was protected with *p*-toluene sulfonyl chloride in a solution of pyridine (25 ml)(Ambrogio & Paride, 2000). After aqueous work up, the white solid (16.8 mmol) obtained was dissolved in pyridine (20 ml) and the resulting solution was refluxed for 6 h. The reaction mixture was concentrated, diluted with 20 mL of 10% sulfuric acid solution and kept in the refrigerator overnight. The pale yellow solid was collected by vacuum filtration and washed with water. After crystallized in 95% ethanol, the title compound was obtained in 75% yield. Crystals suitable for X-ray diffraction analysis were obtained by slow evaporation of a solution in a hexane/ethanol mixture (1: 5 v/v) at room temperature over a period of one week.

Refinement

All H atoms were placed in calculated positions, with C—H = 0.93–0.98 Å, and included in the final cycles of refinement using a riding model, with $U_{iso}(H) = 1.2(1.5 \text{ for methyl groups})$ times $U_{eq}(C)$.

Figures



Fig. 1. The molecular structure of (I), with atom labels and 40% probability displacement ellipsoids for non-H atoms.

5α -androst-2-en-17-one

Crystal data	
C ₁₉ H ₂₈ O	$F_{000} = 600$
$M_r = 272.41$	$D_{\rm x} = 1.142 {\rm ~Mg~m^{-3}}$
Orthorhombic, $P2_12_12_1$	Mo K α radiation $\lambda = 0.71073$ Å
Hall symbol: P 2ac 2ab	Cell parameters from 2794 reflections
a = 6.4725 (17) Å	$\theta = 2.6 - 24.3^{\circ}$
b = 9.003 (2) Å	$\mu = 0.07 \text{ mm}^{-1}$
c = 27.190 (7) Å	T = 298 (2) K
V = 1584.4 (7) Å ³	Block, colourless
Z = 4	$0.41 \times 0.38 \times 0.10 \text{ mm}$

Data collection

Bruker SMART CCD area-detector diffractometer	1650 independent reflections
Radiation source: fine-focus sealed tube	1404 reflections with $I > 2\sigma(I)$
Monochromator: graphite	$R_{\rm int} = 0.033$
T = 293(2) K	$\theta_{\text{max}} = 25.0^{\circ}$
ϕ and ω scans	$\theta_{\min} = 2.4^{\circ}$
Absorption correction: multi-scan (SADABS; Sheldrick, 2004)	$h = -7 \rightarrow 6$
$T_{\min} = 0.973, T_{\max} = 0.993$	$k = -9 \rightarrow 10$
8053 measured reflections	$l = -32 \rightarrow 32$

Refinement

Refinement on F^2	Secondary atom site location: difference Fourier map
Least-squares matrix: full	Hydrogen site location: inferred from neighbouring sites
$R[F^2 > 2\sigma(F^2)] = 0.048$	H-atom parameters constrained
$wR(F^2) = 0.122$	$w = 1/[\sigma^2(F_0^2) + (0.0591P)^2 + 0.212P]$ where $P = (F_0^2 + 2F_c^2)/3$
<i>S</i> = 1.09	$(\Delta/\sigma)_{\rm max} < 0.001$
1650 reflections	$\Delta \rho_{max} = 0.11 \text{ e } \text{\AA}^{-3}$
181 parameters	$\Delta \rho_{min} = -0.13 \text{ e } \text{\AA}^{-3}$

Primary atom site location: structure-invariant direct Extinction correction: none

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc*. and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*-factors based on ALL data will be even larger.

	x	У	Ζ	$U_{\rm iso}*/U_{\rm eq}$
01	0.3020 (3)	0.3005 (3)	-0.01939 (8)	0.0820 (7)
C1	0.8111 (6)	0.8641 (4)	0.22591 (13)	0.0882 (11)
H1A	0.6947	0.8777	0.2479	0.106*
H1B	0.9281	0.8329	0.2457	0.106*
C2	0.8603 (6)	1.0073 (5)	0.2034 (2)	0.1112 (16)
H2A	0.9097	1.0830	0.2235	0.133*
C3	0.8382 (6)	1.0346 (4)	0.15602 (19)	0.0961 (13)
НЗА	0.8738	1.1278	0.1439	0.115*
C4	0.7583 (5)	0.9208 (4)	0.12144 (13)	0.0765 (9)
H4A	0.8741	0.8755	0.1045	0.092*
H4B	0.6731	0.9695	0.0969	0.092*
C5	0.6312 (4)	0.7985 (3)	0.14607 (10)	0.0518 (7)
C6	0.4268 (5)	0.8654 (4)	0.16355 (11)	0.0669 (8)
H6A	0.4542	0.9454	0.1860	0.100*
H6B	0.3468	0.7904	0.1799	0.100*
H6C	0.3512	0.9025	0.1358	0.100*
C7	0.7587 (5)	0.7401 (3)	0.18982 (11)	0.0627 (8)
H7A	0.8906	0.7062	0.1761	0.075*
C8	0.6623 (6)	0.6060 (4)	0.21451 (10)	0.0720 (9)
H8A	0.5322	0.6347	0.2295	0.086*
H8B	0.7532	0.5708	0.2404	0.086*
C9	0.6243 (5)	0.4813 (3)	0.17781 (10)	0.0651 (8)
H9A	0.5555	0.3996	0.1943	0.078*
H9B	0.7558	0.4453	0.1655	0.078*
C10	0.4920 (4)	0.5335 (3)	0.13471 (8)	0.0470 (6)
H10A	0.3568	0.5639	0.1474	0.056*
C11	0.5946 (4)	0.6690 (3)	0.11010 (9)	0.0471 (6)
H11A	0.7325	0.6354	0.1002	0.057*
C12	0.4858 (5)	0.7149 (3)	0.06213 (10)	0.0626 (8)
H12A	0.3522	0.7574	0.0701	0.075*
H12B	0.5671	0.7912	0.0460	0.075*
C13	0.4550 (5)	0.5864 (4)	0.02671 (9)	0.0649 (8)
H13A	0.3785	0.6201	-0.0019	0.078*
H13B	0.5882	0.5499	0.0157	0.078*
C14	0.3375 (4)	0.4628 (3)	0.05196 (9)	0.0526 (7)
C15	0.1143 (4)	0.5095 (4)	0.06359 (11)	0.0693 (9)
H15A	0.0468	0.5403	0.0338	0.104*
H15B	0.1156	0.5904	0.0866	0.104*

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (A^2)

supplementary materials

H15C	0.0411	0.4270	0.0776	0.104*
C16	0.4598 (4)	0.4119 (3)	0.09699 (9)	0.0492 (6)
H16A	0.5976	0.3852	0.0850	0.059*
C17	0.3560 (5)	0.2663 (3)	0.11169 (11)	0.0661 (8)
H17A	0.2301	0.2842	0.1301	0.079*
H17B	0.4480	0.2050	0.1312	0.079*
C18	0.3094 (6)	0.1936 (4)	0.06180 (12)	0.0723 (9)
H18A	0.4127	0.1190	0.0541	0.087*
H18B	0.1746	0.1465	0.0623	0.087*
C19	0.3143 (4)	0.3164 (4)	0.02465 (11)	0.0620 (8)

Atomic displacement parameters (\AA^2)

	U^{11}	U^{22}	U ³³	U^{12}	U^{13}	U^{23}
01	0.0697 (14)	0.1079 (19)	0.0685 (14)	0.0052 (15)	-0.0087 (11)	-0.0295 (13)
C1	0.081 (2)	0.091 (3)	0.092 (2)	-0.010 (2)	-0.015 (2)	-0.024 (2)
C2	0.071 (2)	0.079 (3)	0.184 (5)	-0.009 (2)	-0.019 (3)	-0.057 (3)
C3	0.078 (2)	0.062 (2)	0.149 (4)	-0.019 (2)	-0.018 (3)	0.000 (3)
C4	0.066 (2)	0.0559 (19)	0.107 (2)	-0.0104 (18)	0.0156 (18)	0.0012 (19)
C5	0.0449 (14)	0.0461 (15)	0.0644 (16)	-0.0005 (13)	0.0067 (12)	-0.0033 (13)
C6	0.0615 (19)	0.0570 (18)	0.0823 (19)	0.0043 (15)	0.0080 (15)	-0.0150 (16)
C7	0.0557 (17)	0.0626 (19)	0.0698 (18)	-0.0004 (15)	-0.0044 (15)	-0.0127 (15)
C8	0.085 (2)	0.074 (2)	0.0567 (16)	-0.005 (2)	-0.0179 (16)	0.0033 (16)
C9	0.083 (2)	0.0537 (18)	0.0583 (16)	-0.0008 (17)	-0.0112 (16)	0.0081 (14)
C10	0.0455 (14)	0.0462 (15)	0.0493 (13)	0.0007 (12)	0.0044 (12)	0.0025 (11)
C11	0.0385 (13)	0.0492 (15)	0.0536 (13)	0.0037 (12)	0.0086 (11)	0.0036 (12)
C12	0.0679 (18)	0.0579 (18)	0.0621 (16)	-0.0027 (16)	0.0023 (15)	0.0161 (15)
C13	0.0693 (19)	0.079 (2)	0.0459 (14)	0.0017 (18)	-0.0020 (14)	0.0064 (15)
C14	0.0454 (15)	0.0604 (17)	0.0522 (14)	0.0060 (13)	-0.0016 (13)	-0.0045 (13)
C15	0.0480 (16)	0.078 (2)	0.082 (2)	0.0116 (16)	-0.0071 (14)	-0.0115 (18)
C16	0.0474 (14)	0.0460 (15)	0.0543 (14)	0.0051 (13)	0.0031 (12)	-0.0010 (12)
C17	0.071 (2)	0.0486 (16)	0.0788 (19)	-0.0050 (16)	-0.0074 (17)	0.0013 (15)
C18	0.068 (2)	0.0572 (19)	0.092 (2)	-0.0002 (17)	-0.0068 (18)	-0.0157 (18)
C19	0.0412 (15)	0.077 (2)	0.0679 (19)	0.0089 (16)	-0.0075 (13)	-0.0182 (17)

Geometric parameters (Å, °)

O1—C19	1.209 (3)	C10—C16	1.515 (3)
C1—C2	1.462 (6)	C10-C11	1.541 (3)
C1—C7	1.525 (4)	C10—H10A	0.9800
C1—H1A	0.9700	C11—C12	1.539 (4)
C1—H1B	0.9700	C11—H11A	0.9800
C2—C3	1.320 (6)	C12—C13	1.518 (4)
C2—H2A	0.9300	C12—H12A	0.9700
C3—C4	1.484 (5)	C12—H12B	0.9700
С3—НЗА	0.9300	C13—C14	1.513 (4)
C4—C5	1.529 (4)	C13—H13A	0.9700
C4—H4A	0.9700	C13—H13B	0.9700
C4—H4B	0.9700	C14—C19	1.520 (4)

C5—C6	1.529 (4)	C14—C16	1.528 (4)
C5—C11	1.540 (4)	C14—C15	1.538 (4)
C5—C7	1.541 (4)	C15—H15A	0.9600
С6—Н6А	0.9600	C15—H15B	0.9600
С6—Н6В	0.9600	C15—H15C	0.9600
С6—Н6С	0.9600	C16—C17	1.526 (4)
С7—С8	1.516 (4)	C16—H16A	0.9800
С7—Н7А	0.9800	C17—C18	1.536 (4)
C8—C9	1.522 (4)	C17—H17A	0.9700
C8—H8A	0.9700	C17—H17B	0.9700
C8—H8B	0.9700	C18—C19	1.498 (5)
C9—C10	1.525 (4)	C18—H18A	0.9700
С9—Н9А	0.9700	C18—H18B	0.9700
С9—Н9В	0.9700		
$C^{2}-C^{1}-C^{7}$	115 2 (3)	C11—C10—H10A	108 5
$C_2 = C_1 = H_1 A$	108 5	C_{12} C_{11} C_{12} C_{11} C_{12} C_{12} C_{11} C_{12} C_{12} C_{11} C_{12} C	100.5 113.9(2)
C7-C1-H1A	108.5	$C_{12} = C_{11} = C_{10}$	113.5(2)
C^2 C^1 H^1B	108.5	C_{5} C_{11} C_{10}	112.0(2)
$C_2 = C_1 = H_1 B$	108.5	$C_{12} = C_{11} = H_{11A}$	105.5
	108.5	C5 C11 H11A	105.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	107.3 122.2 (4)		105.5
C_{2} C_{2} U_{2}	123.3 (4)	C_{10} C_{12} C_{12} C_{11}	103.3
C_{3} C_{2} H_{2}	110.4	$C_{12} = C_{12} = C_{11}$	115.1 (2)
C1 - C2 - R2A	110.4	C13 - C12 - H12A	109.0
$C_2 = C_3 = C_4$	121.9 (4)	CII—CI2—HI2A	109.0
C2—C3—H3A	119.0	C13-C12-H12B	109.0
C4—C3—H3A	119.0		109.0
C3—C4—C5	114.0 (3)	H12A—C12—H12B	107.8
C3—C4—H4A	108.7	C14—C13—C12	109.8 (2)
C5—C4—H4A	108.7	С14—С13—Н13А	109.7
C3—C4—H4B	108.7	С12—С13—Н13А	109.7
C5—C4—H4B	108.7	С14—С13—Н13В	109.7
H4A—C4—H4B	107.6	С12—С13—Н13В	109.7
C4—C5—C6	108.5 (2)	H13A—C13—H13B	108.2
C4—C5—C11	110.5 (2)	C13—C14—C19	117.8 (2)
C6—C5—C11	111.3 (2)	C13—C14—C16	108.9 (2)
C4—C5—C7	107.2 (2)	C19—C14—C16	100.5 (2)
C6—C5—C7	111.0 (2)	C13—C14—C15	111.3 (3)
C11—C5—C7	108.3 (2)	C19—C14—C15	104.2 (2)
С5—С6—Н6А	109.5	C16C14C15	113.8 (2)
С5—С6—Н6В	109.5	C14—C15—H15A	109.5
H6A—C6—H6B	109.5	C14—C15—H15B	109.5
С5—С6—Н6С	109.5	H15A—C15—H15B	109.5
H6A—C6—H6C	109.5	C14—C15—H15C	109.5
H6B—C6—H6C	109.5	H15A—C15—H15C	109.5
C8—C7—C1	112.9 (3)	H15B—C15—H15C	109.5
C8—C7—C5	113.1 (3)	C10—C16—C17	120.3 (2)
C1—C7—C5	111.5 (3)	C10-C16-C14	113.4 (2)
C8—C7—H7A	106.2	C17—C16—C14	103.9 (2)
C1—C7—H7A	106.2	C10-C16-H16A	106.1

supplementary materials

С5—С7—Н7А	106.2	C17—C16—H16A	106.1
C7—C8—C9	111.3 (2)	C14—C16—H16A	106.1
С7—С8—Н8А	109.4	C16—C17—C18	102.8 (2)
С9—С8—Н8А	109.4	С16—С17—Н17А	111.2
С7—С8—Н8В	109.4	С18—С17—Н17А	111.2
С9—С8—Н8В	109.4	С16—С17—Н17В	111.2
H8A—C8—H8B	108.0	С18—С17—Н17В	111.2
C8—C9—C10	111.5 (2)	H17A—C17—H17B	109.1
С8—С9—Н9А	109.3	C19—C18—C17	106.1 (2)
С10—С9—Н9А	109.3	C19—C18—H18A	110.5
С8—С9—Н9В	109.3	C17—C18—H18A	110.5
С10—С9—Н9В	109.3	C19—C18—H18B	110.5
Н9А—С9—Н9В	108.0	C17—C18—H18B	110.5
C16—C10—C9	112.0 (2)	H18A—C18—H18B	108.7
C16—C10—C11	109.71 (19)	O1—C19—C18	125.4 (3)
C9—C10—C11	109.6 (2)	O1—C19—C14	126.4 (3)
C16-C10-H10A	108.5	C18—C19—C14	108.2 (2)
C9—C10—H10A	108.5		
C7—C1—C2—C3	7.8 (6)	C9—C10—C11—C5	-57.1 (3)
C1—C2—C3—C4	0.7 (7)	C5-C11-C12-C13	178.8 (2)
C2—C3—C4—C5	22.1 (6)	C10-C11-C12-C13	-51.0 (3)
C3—C4—C5—C6	70.0 (4)	C11—C12—C13—C14	55.8 (3)
C3—C4—C5—C11	-167.8 (3)	C12—C13—C14—C19	-172.6 (2)
C3—C4—C5—C7	-50.0 (4)	C12-C13-C14-C16	-59.1 (3)
C2—C1—C7—C8	-166.8 (3)	C12—C13—C14—C15	67.3 (3)
C2—C1—C7—C5	-38.1 (4)	C9-C10-C16-C17	59.4 (3)
C4—C5—C7—C8	-173.6 (2)	C11-C10-C16-C17	-178.7 (2)
C6—C5—C7—C8	68.1 (3)	C9-C10-C16-C14	-176.9 (2)
C11—C5—C7—C8	-54.4 (3)	C11-C10-C16-C14	-55.0 (3)
C4—C5—C7—C1	57.8 (3)	C13-C14-C16-C10	60.9 (3)
C6—C5—C7—C1	-60.5 (3)	C19—C14—C16—C10	-174.8 (2)
C11—C5—C7—C1	177.1 (3)	C15-C14-C16-C10	-64.0 (3)
C1—C7—C8—C9	-176.6 (3)	C13-C14-C16-C17	-166.9 (2)
C5—C7—C8—C9	55.6 (4)	C19—C14—C16—C17	-42.5 (3)
C7—C8—C9—C10	-55.8 (4)	C15-C14-C16-C17	68.3 (3)
C8—C9—C10—C16	177.9 (2)	C10-C16-C17-C18	167.3 (2)
C8—C9—C10—C11	55.9 (3)	C14—C16—C17—C18	39.1 (3)
C4—C5—C11—C12	-57.5 (3)	C16-C17-C18-C19	-19.9 (3)
C6—C5—C11—C12	63.1 (3)	C17—C18—C19—O1	173.4 (3)
C7—C5—C11—C12	-174.6 (2)	C17-C18-C19-C14	-6.6 (3)
C4—C5—C11—C10	172.5 (2)	C13-C14-C19-O1	-31.7 (4)
C6—C5—C11—C10	-66.9 (3)	C16-C14-C19-O1	-149.8 (3)
C7—C5—C11—C10	55.4 (3)	C15-C14-C19-O1	92.1 (3)
C16—C10—C11—C12	48.9 (3)	C13-C14-C19-C18	148.2 (3)
C9—C10—C11—C12	172.2 (2)	C16-C14-C19-C18	30.1 (3)
C16-C10-C11-C5	179.5 (2)	C15-C14-C19-C18	-88.0 (3)



Fig. 1